

APPENDIX 4

SUB-SURFACE INVESTIGATION - DYKES

TABLE OF CONTENTS

	<u>Page</u>
1. GENERAL	4 - 1
2. FIELD EXPLORATION	4 - 1
3. STRATA	4 - 2
4. FIELD PERMEABILITY	4 - 3
5. LABORATORY TESTING	4 - 4
a. Gradations	4 - 4
b. Atterberg Limits	4 - 4

SUB-SURFACE INVESTIGATION - DYKES1. General

A sub-surface investigation was carried out along the Vedder Canal and Lower Sumas River dykes during the period January to May 1977. This investigation, which consisted of drill holes, in situ permeability testing and laboratory testing, was made to obtain sufficient information for the First Stage - Final Design of the dykes. The 1977 work supplemented earlier investigations carried out in 1918, 1948, 1963, and 1970 (4, 7, 18 - 22) \*

2. Field Exploration

Thirteen holes were drilled by rotary methods at the locations shown on Fig. 4.1. The depths of the drill holes and descriptions of the soils encountered are given on the attached logs.

In general, disturbed and undisturbed soil samples were taken at 1.5 m (4.9 ft) intervals or at changes in soil type. Standard penetration tests were carried out in granular material by driving a 35 mm (1.4 in.) dia split sampling spoon. Undisturbed samples of the silt were obtained by means of hydraulically advanced 85 mm (3.3 in.) Shelby tubes. Prior to waxing the undisturbed samples, shear strength tests were carried out on any silt exposed in the bottom of the tubes using a "Torvane".

\* These references are listed in Volume 1, Section 9.

Falling head permeability tests were carried out in several of the drill holes. Standpipe piezometers were installed in all the drill holes.

The results of the penetration, strength and permeability tests carried out in the field are given on the drill hole logs.

The drilling was carried out by Keller Soiltest Drilling Ltd. using a Mayhew 1000 rotary drill rig.

### 3. Strata

A profile along the dyke showing the soil strata encountered in the drill holes is given on Fig. 4.2.

The foundation soils beneath the dyke generally comprise a series of lacustrine and river flood plain deposits of silt and clay, and fine sand, except at the east end of the Vedder River dyke where fluvial sand and gravel is superimposed upon the lacustrine deposits.

Sand and gravel was encountered beneath the Vedder dykes in the holes drilled between Sta 0+00 (B. C. Hydro Railway) and approximately Sta 10+00 (First Street, Yarrow). The sand and gravel was encountered to the maximum depth of drill hole 3 of 14 m (50 ft) below natural ground level. The sand and gravel is overlain by 1.0 to 1.5 m (3.3 to 4.9 ft) of fine sand and minor silt.

Between Sta 10+00 and Sta 51+80 approximately the dyke is directly underlain by silty fine and fine to medium sand with

minor silt layers and with some coarse sand and occasional traces of organics. This material was encountered to the maximum depth of the drill holes of about 14 m (50 ft) below natural ground level. Previous investigations indicate that some zones of silt with layers of sand may be present within this stratum.

The dyke is directly underlain by a layer of silt or silt with fine sand, from 1.5 to 5 m (4.9 to 16.4 ft) in thickness between Sta 51+80 and Sumas Pump Station. This deposit is underlain by the stratum of sand with silty layers encountered from Sta 10+00 to 51+80 approximately and described above. The sand was encountered to the maximum depth of the drill holes of about 13 m (43 ft) below natural ground level.

The Vedder dyke fill generally consists of fine to coarse silty sand with minor layers or lenses of sandy silt. The dyke fill upstream of about First Street, Yarrow, is generally sand with some gravel. The Lower Sumas River dyke fill consists of fine sand with silt.

Groundwater levels measured in the drill holes each day prior to drilling were generally less than 1.0 m (3.3 ft) below natural ground level on the landside of the dykes.

#### 4. Field Permeability

Falling head permeability tests were carried out in the foundation soils in several of the drill holes. The holes were drilled ahead of the casing for 2 to 3 m (7 to 10 ft), washed out with clean water and the rate of fall of the water level was measured and the permeabilities evaluated. The in-situ permeability values

measured are given on the drill hole logs. The calculated values range from  $0.5 \times 10^{-4}$  to  $5 \times 10^{-4}$  cm/sec.

In several of the holes permeability tests could not be carried out because the casing was loose in the hole and drill fluid returned outside the casing.

Several grain size analyses were carried out on samples in the vicinity of in-situ permeability tests. No correlation between grain size distribution and permeability is evident. This may be expected due to the variable nature of the soils and because the permeability test gives an average value over some 2 to 3 m (7 to 10 ft) of hole.

## 5. Laboratory Testing

### a. Gradations

The gradations of several samples of the dyke fill and foundation soil were determined and the results are given in Table 4.1 and on Figs. 4.3 to 4.11.

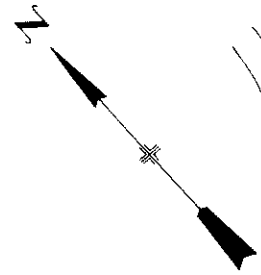
### b. Atterberg Limits

As will be noted from Table 4.1, all except one of the representative samples selected for Atterberg limit testing proved to be non-plastic and the exception is a silt of low plasticity.

TABLE 4.1  
 ABBOTSFORD PROJECT - DYKES  
 RESULTS OF LABORATORY TESTS

Drill Hole No.	Sample Depth m	Index Properties			Grain Size Distribution			Remarks
		Liquid Limit %	Plastic Limit %	Plasticity Index %	Sand %	Silt %	Clay %	
3	1.5	-	-		80		4	
4	1.5*	-	-		89	9	0	(2% gravel)
	7.6	-	-		91	9	0	
6	1.5	-	-		56	24	9	(11% gravel)
8	2.1	-	-		28	67	<5	
9	1.5	-	-		69	26	5	
10	3.0*	-	-		93	7	0	
11	5.0	-	-		89	9	<2	
12	10.7	-	-		71	25	4	
13	1.5	43	26	17	<10	75	<15	

\* These samples from dyke fill material, all others are from dyke foundation.

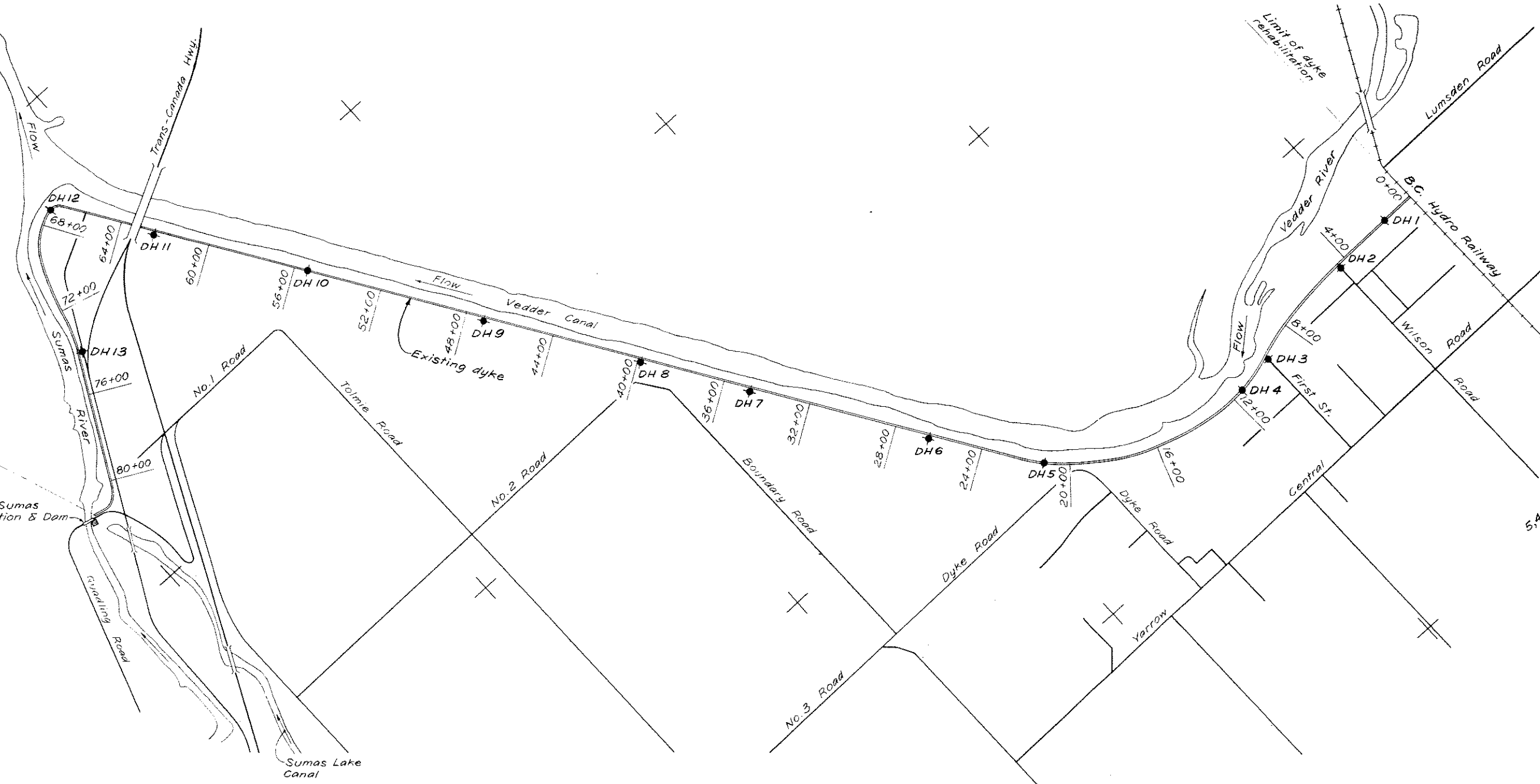


5,442,000 N  
565,000 E

5,441,000 N  
564,000 E

571,000 E  
5,437,000 N

570,000 E  
5,436,000 N

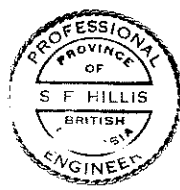


**LEGEND :**

◆ DH 5 Drillhole

**NOTES**

1. All stations in metres.
2. Drillholes 1, 4, 5, 10 & 12 drilled from crest of dyke.  
Drillholes 2, 3, 6, 7, 8, 9, 11 & 13 drilled from landside toe of dyke.



**CRIPPEN ENGINEERING LTD.**  
NORTH VANCOUVER, B.C.  
PROJECT NO. 10407

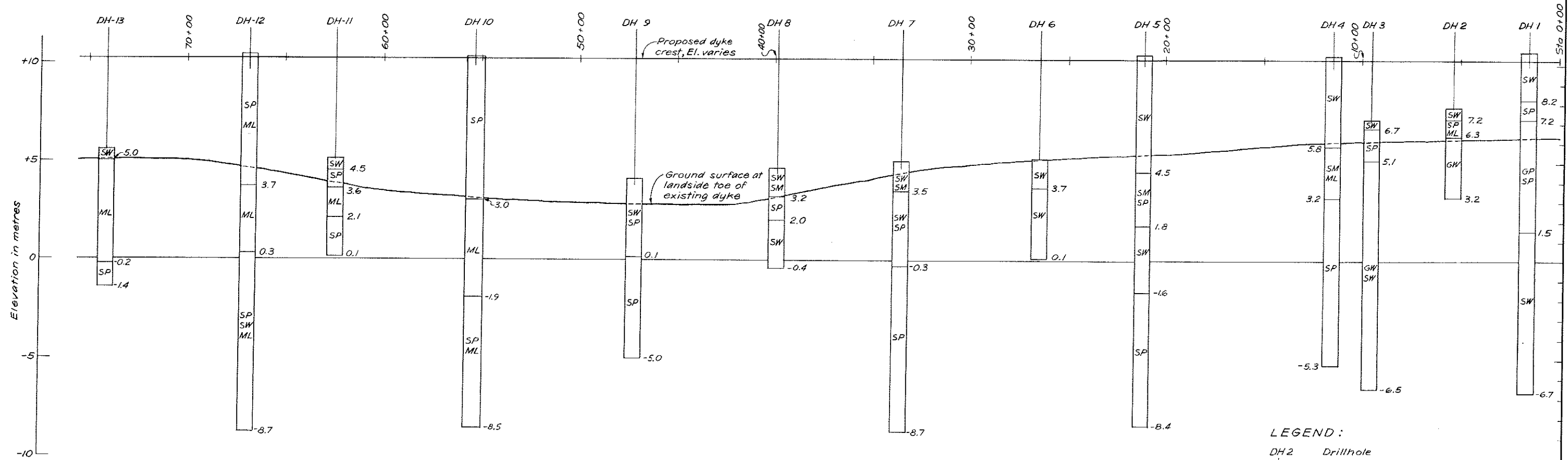
DEPARTMENT HEAD: *S.F. Hillis*  
PROJECT ENGINEER: *John A. Bird*  
CHIEF ENGINEER: *John S. Huber*

NO.	DESCRIPTION	BY	CHKD	APPR	DATE

RECOMMENDED	PROJECT MANAGER	BRITISH COLUMBIA MINISTRY OF THE ENVIRONMENT WATER INVESTIGATIONS BRANCH CANADA-BRITISH COLUMBIA FRASER RIVER FLOOD CONTROL 1968 AGREEMENT PROJECT NO. 8 <b>DYKE REHABILITATION</b> <b>LOCATION OF DRILLHOLES</b>	DESIGNED: <i>John Lumb</i>	SURVEYED
DATE			DRAWN: A.A.	DATE
APPROVED	DIRECTOR, WATER INVESTIGATIONS		CHECKED: SFH	FILE NO.
DATE			SCALE: As shown	DATE
			DWG. NO. 4844-PR-D25	SHEET OF SHEETS

FIG. 4.





**LEGEND :**

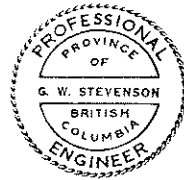
DH 2 Drillhole

SW 8.2 Soil type  
 SP 6.3 Elevation in m

**Soil Type**  
 ML - Inorganic silt, low plasticity  
 SM - Silty sand  
 SW - Well graded sand with little or no fines  
 SP - Poorly graded sand with little or no fines  
 GW - Well graded gravel with little or no fines, gravel-sand mixtures  
 GP - Poorly graded gravel with little or no fines

**NOTES :**

1. All stations in metres.
2. For location of drillholes see Dwg. D 25.



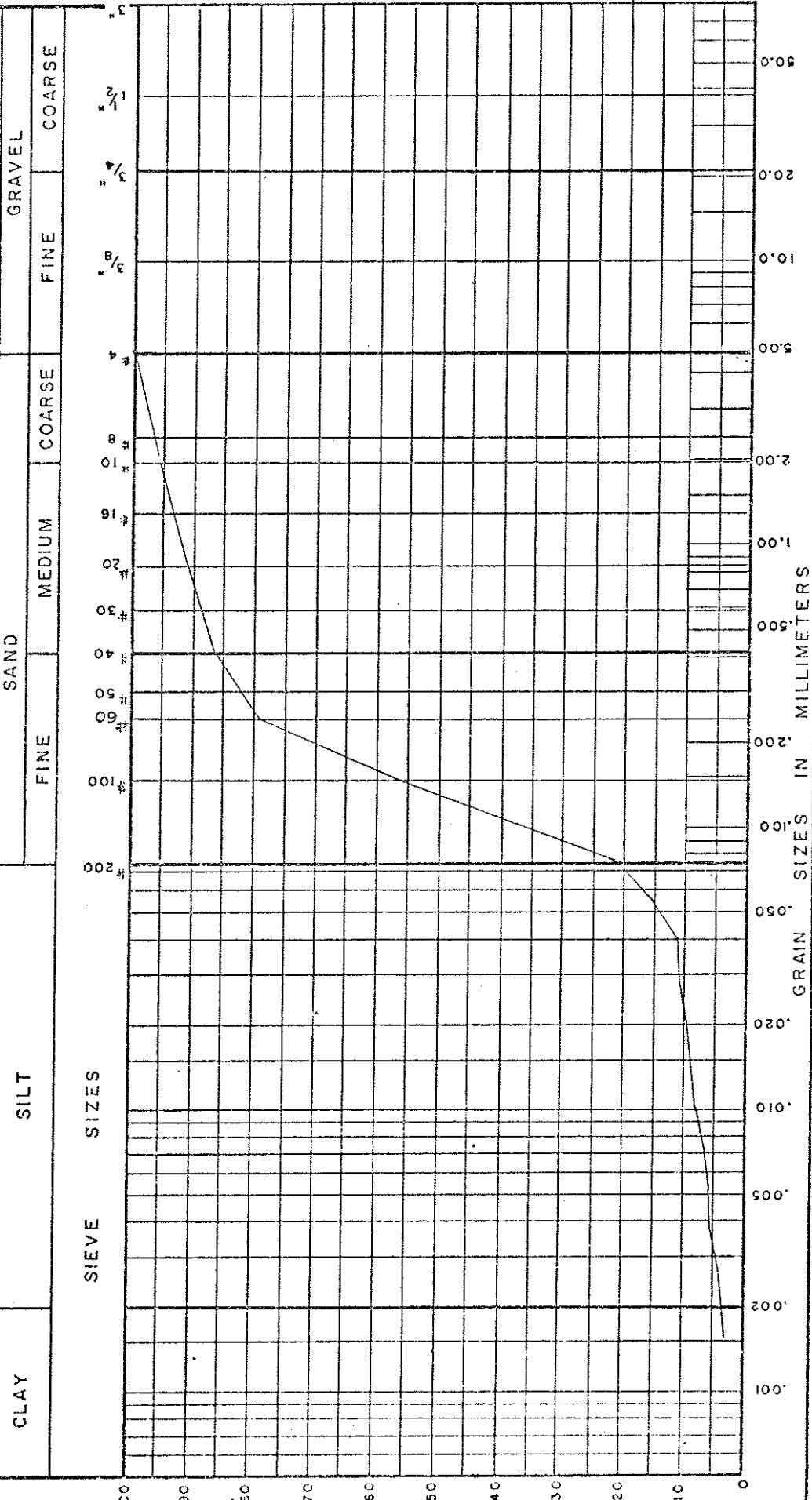
**CRIPPEN ENGINEERING LTD.**  
 NORTH VANCOUVER, B.C.  
 PROJECT NO. 10407  
 DEPARTMENT HEAD: S.F. Hillen  
 PROJECT ENGINEER: [Signature]  
 CHIEF ENGINEER: [Signature]

NO.	DESCRIPTION	BY	CHK	APPR	DATE

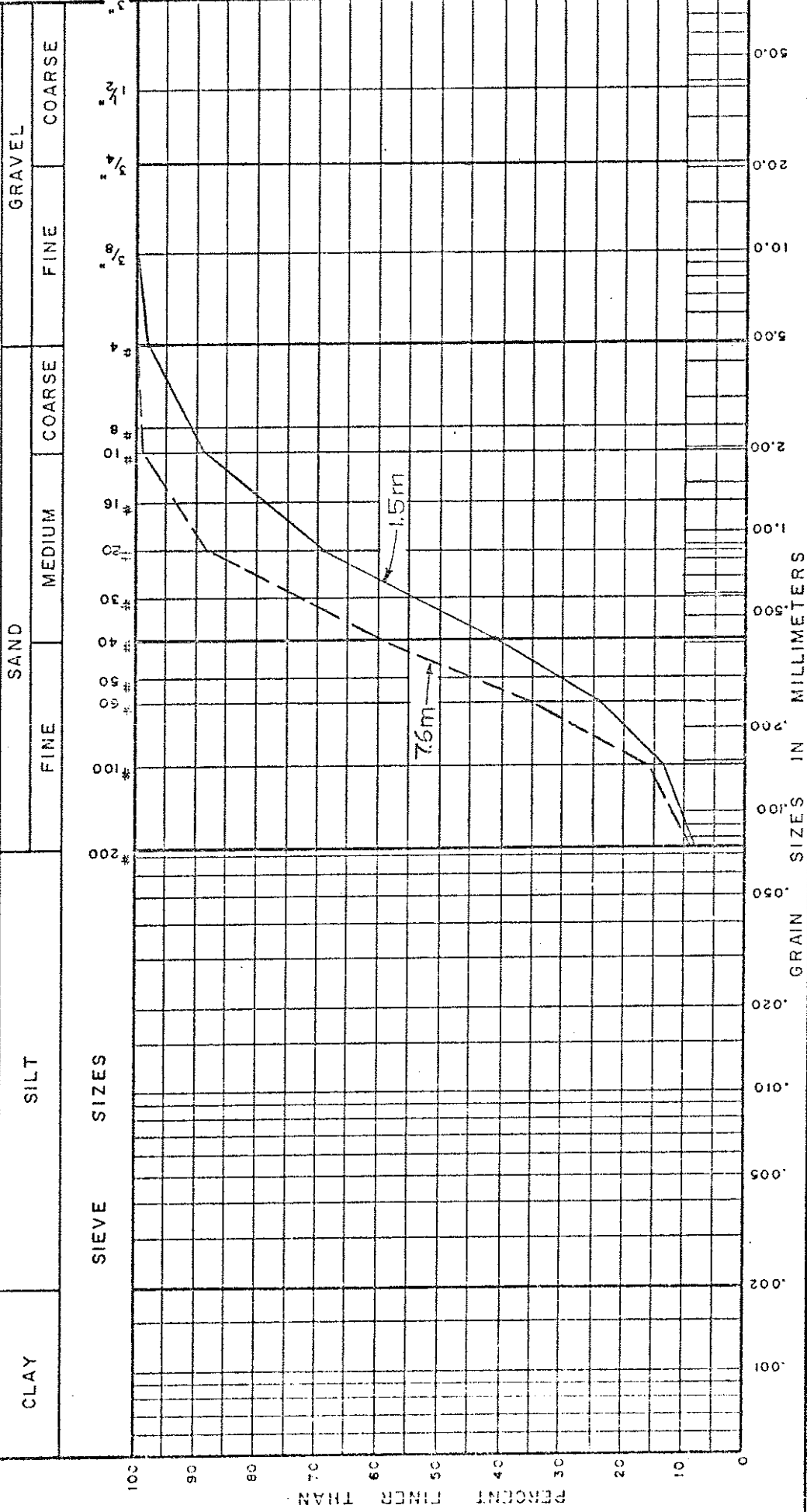
RECOMMENDED PROJECT MANAGER	BRITISH COLUMBIA MINISTRY OF THE ENVIRONMENT WATER INVESTIGATIONS BRANCH CANADA - BRITISH COLUMBIA FRASER RIVER FLOOD CONTROL 1968 AGREEMENT	DESIGNED H.W. [Signature]	SURVEYED
DATE	PROJECT NO. 8 ABBOTSFORD PROJECT	DRAWN HDVT	DATE
APPROVED DIRECTOR, WATER INVESTIGATIONS	DYKE REHABILITATION	CHECKED GWS	FILE NO. 0281550 - B24
DATE	SOIL PROFILE ALONG CENTRE-LINE OF DYKE	SCALE As shown	DATE 8 June 1977
		DWG. NO. 4844-PR-D26	SHEET OF SHEETS

FIG. 4.2

UNIFIED SOIL CLASSIFICATION SYSTEM & N.R.C. FIELD DESCRIPTION (MODIFIED WITH CLAY SIZES AT .002 m.m.)

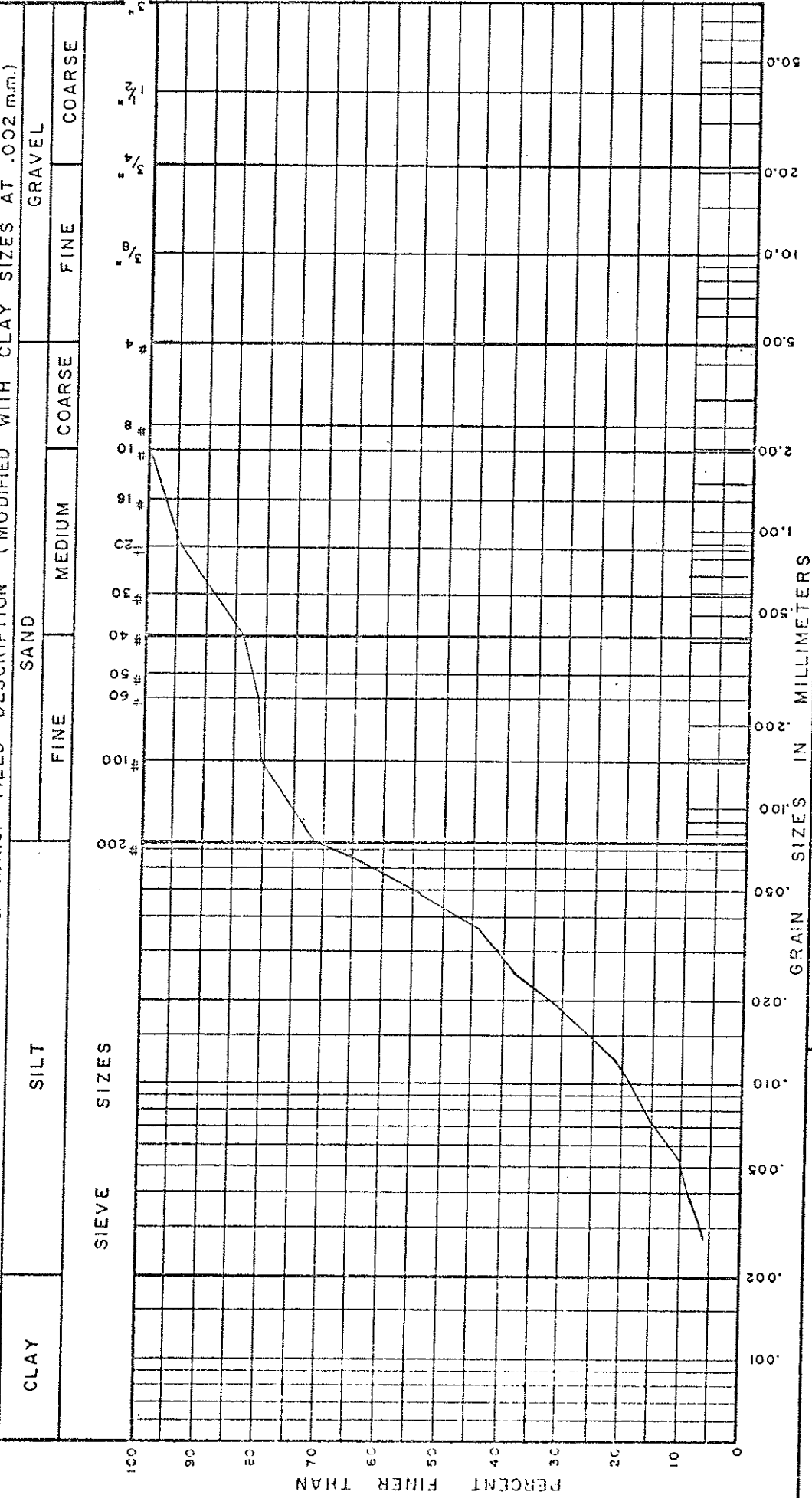


UNIFIED SOIL CLASSIFICATION SYSTEM & N.R.C. FIELD DESCRIPTION (MODIFIED WITH CLAY SIZES AT .002 mm.)





UNIFIED SOIL CLASSIFICATION SYSTEM & N.R.C. FIELD DESCRIPTION (MODIFIED WITH CLAY SIZES AT .002 mm.)



REMARKS

CRIPPEN ENGINEERING LTD

GRAIN SIZE DISTRIBUTION

PROJECT --- ABBOTSFORD DYKES ---

HOLE NO. --- DH8 ---

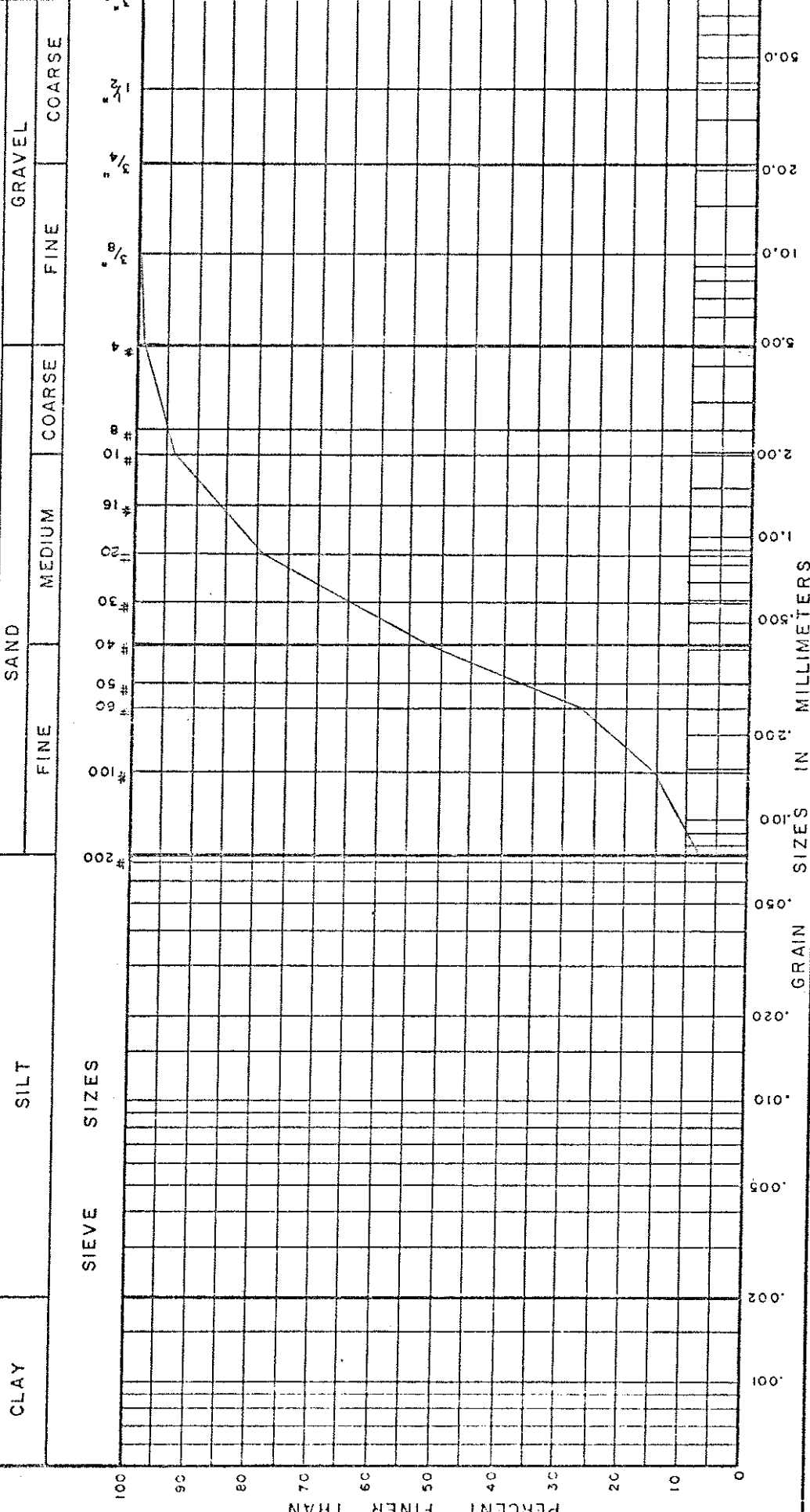
DEPTH --- 2.1 m. ---

MATERIAL --- Sandy Silt ---

COMPILED BY GWS --- Fig. 4.6 ---



UNIFIED SOIL CLASSIFICATION SYSTEM & N.R.C. FIELD DESCRIPTION (MODIFIED WITH CLAY SIZES AT .002 m.m.)



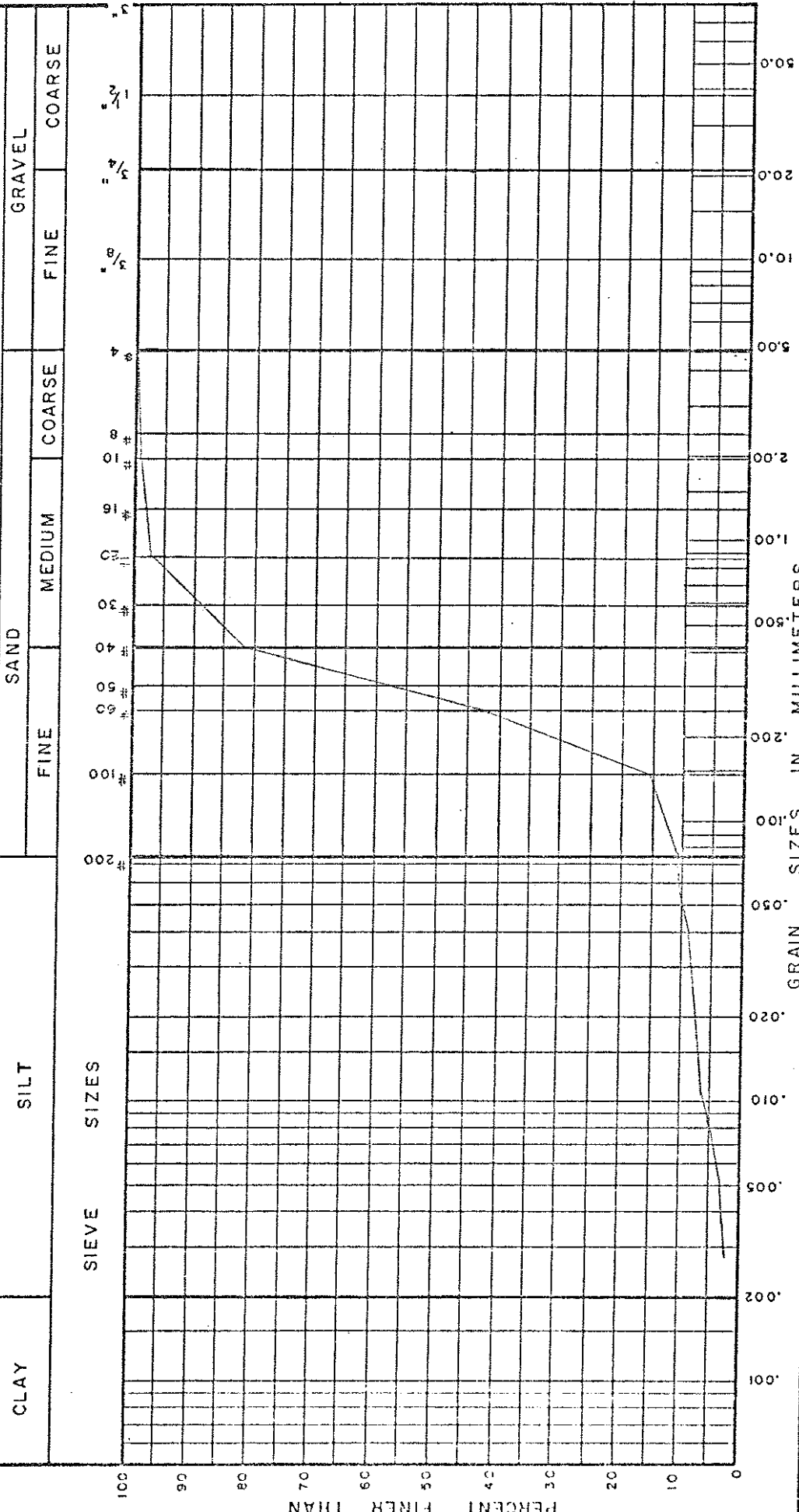
CRIPPEN ENGINEERING LTD

GRAIN SIZE DISTRIBUTION

REMARKS -----  
 -----  
 -----  
 -----

PROJECT --- ABBOTSFORD DYKES ---  
 HOLE NO. --- DH10 ---  
 DEPTH --- 3.0m ---  
 MATERIAL --- Sand ---  
 COMPILED BY --- GWS --- Fig. A.2 ---

UNIFIED SOIL CLASSIFICATION SYSTEM & N.R.C. FIELD DESCRIPTION (MODIFIED WITH CLAY SIZES AT .002 m.m.)



REMARKS

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GRAIN SIZE DISTRIBUTION

PROJECT --- ABBOTSFORD DYKES

HOLE NO. --- DH11

DEPTH --- 5.0m

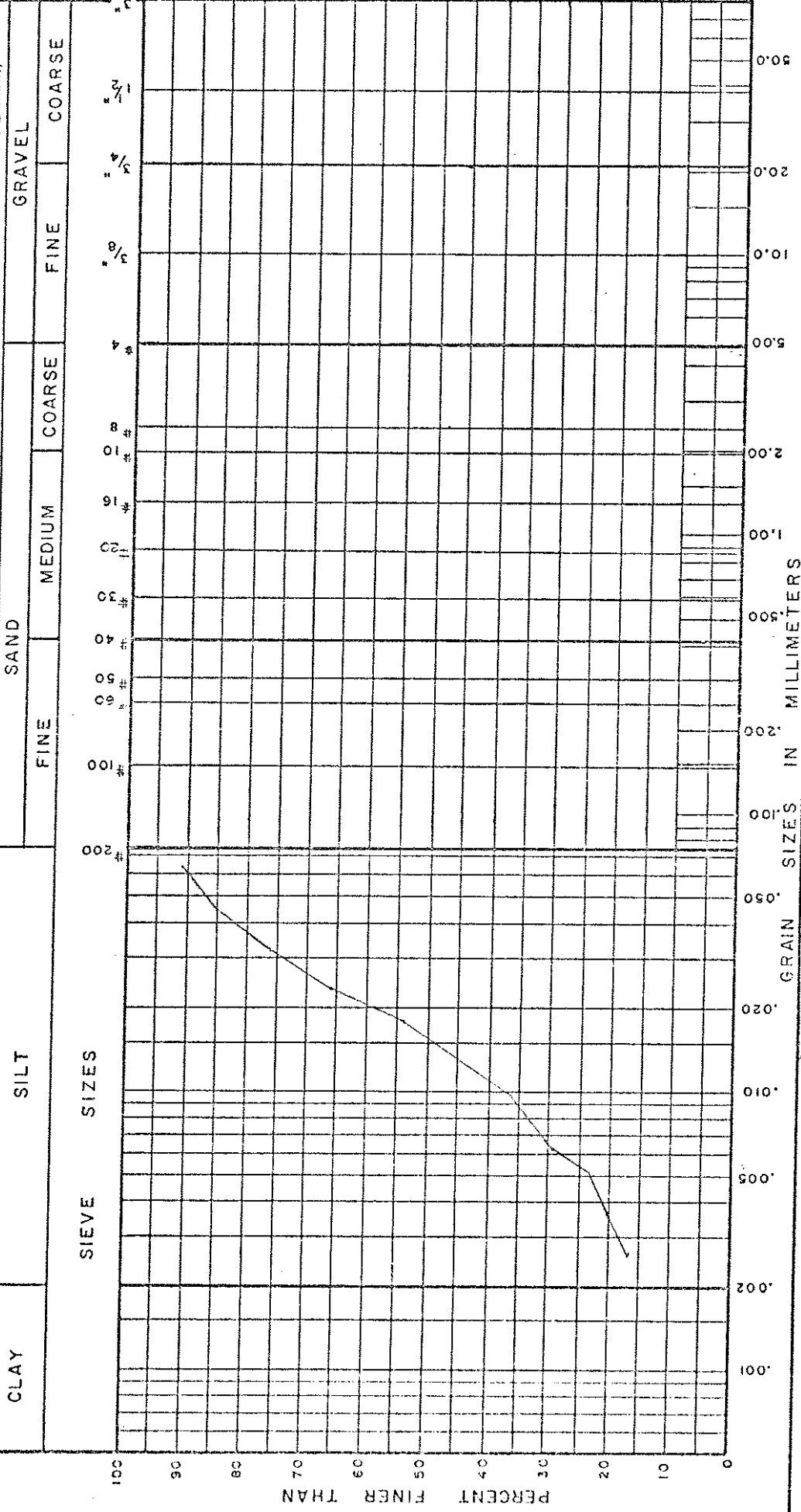
MATERIAL --- Fine Sand

COMPILED BY --- G.W.S. --- Fig. 4.9





UNIFIED SOIL CLASSIFICATION SYSTEM & N.R.C. FIELD DESCRIPTION (MODIFIED WITH CLAY SIZES AT .002 m.m.)



REMARKS

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GRAIN SIZE DISTRIBUTION

PROJECT --- ABBOTSFORD DYKES ---

HOLE NO. --- DH13 ---

DEPTH --- 1.5m ---

MATERIAL --- Silt ---

COMPILED BY GWS --- Fig. 4-11 ---



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## LOG OF DRILL HOLE

HOLE NO. DH 1  
SHEET 1 OF 1

PROJECT ABBOTSFORD  
LOCATION OF HOLE Chainage  
1+53.5  
ELEVATION 10.64  
CONTRACTOR Keller Soiltest  
TYPE OF DRILL Mayhew 1000  
DATE OF DRILLING 7 - 9 Feb 1977

### LEGEND

- SPLIT SPOON
- WASH SAMPLE
- SHELBY TUBE
- CORE SAMPLE

### SHEAR STRENGTH

- UNCONFINED COMPRESSION
- TORVANE
- PENETRATION RESISTANCE
- STANDARD N - VALUE
- ATTERBERG LIMITS

P.L. 
←
→
 L.L.  
MOISTURE CONTENT

SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS								SAMPLE NO.	RECOVERY cm		
				10	20	30	40	50	60	70	80			kN/m <sup>2</sup>	BLOWS/FT. (0.3 m)
SW	SAND, medium to coarse, gravelly														
	FILL	2.4	8.2												5/45
SP	SAND, silty, fine with thin layers of silt	3.4	7.2												13/45
GP	GRAVEL, sandy and														0/45
SP	SAND, gravelly, coarse Little or no fine sand and silt	6													0/45
		8													8/45
SW	SAND, well-graded, medium to coarse. Silt layers at 9.1 to 9.8 and 13.4 to 14.3 m; elsewhere, occasional thin layers of silt	9.1	1.5												10/45
		12													30/45
		14													45/45
	Sample at 16.8 m was gravelly sand.	16													45/45
		17.3	-6.7												0/45
															25/45
	Bottom of hole, elev -6.7														
	Installed piezometer, tip at depth 6.5 to 7.4 m														
	No permeability test, as casing was loose in hole to 9 m (losing water down side of casing and out bottom of casing)														
	Very hard driving and cleaning out casing to 9 m														
	Used Revert mud to 9 m, water to 12 m, drill mud to 17 m														
	Used casing to 11 m														



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## LOG OF DRILL HOLE

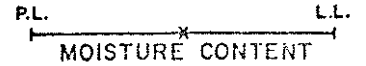
HOLE NO. DH 2  
SHEET 1 OF 1

PROJECT ABBOTSFORD  
LOCATION OF HOLE Chainage  
4+35.1  
ELEVATION 7.83  
CONTRACTOR Keller Soiltest  
TYPE OF DRILL Mayhew 1000  
DATE OF DRILLING 4 Feb 1977

### LEGEND

- SPLIT SPOON
- WASH SAMPLE
- SHELBY TUBE
- CORE SAMPLE

- SHEAR STRENGTH
- UNCONFINED COMPRESSION
- TORVANE
- PENETRATION RESISTANCE
- STANDARD N-VALUE
- ATTERBERG LIMITS



SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS								SAMPLE NO.	RECOVERY cm		
				10	20	30	40	40	60	80	80				
				kN/m <sup>2</sup>				BLOWS/FT. (0.3m)							
SW	SAND, medium to coarse, gravelly, Fill	0.6	7.2												
SP, ML	SAND, fine and SILT, brown	1.5	6.3												20/45
GM	GRAVEL, sandy, silty More sandy below 3 m depth	4													
	Bottom of hole, elev 3.2 Installed standpipe piezometer, tip at depth 1.8 to 2.7 m	4.6	3.2												
	Had great difficulty advancing casing beyond 1.5 m - ground kept caving - gravel and coarse sand jammed between casing and drill rod - tried 3 times to advance casing to 3 m														
	Advanced drill to 4.6 m without casing and without sampling - ground was very loose judging from drill advance rate - hole caved immediately behind drill														
	No permeability test attempted, as water was returning around casing														



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## LOG OF DRILL HOLE

HOLE NO. DH 3  
SHEET 1 OF 1

PROJECT ABBOTSFORD  
LOCATION OF HOLE Chainage  
9+50.3  
ELEVATION 7.20  
CONTRACTOR Keller Soiltest  
TYPE OF DRILL Mayhew 1000  
DATE OF DRILLING 4 Feb 1977

### LEGEND

- ☒ SPLIT SPOON
- ☒ WASH SAMPLE
- ☒ SHELBY TUBE
- ☐ CORE SAMPLE

- ### SHEAR STRENGTH
- ⊕ UNCONFINED COMPRESSION
  - + TORVANE
- ### PENETRATION RESISTANCE
- ⊙ STANDARD N-VALUE
- ### ATTERBERG LIMITS



SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS				SAMPLE NO.	RECOVERY cm
				10	20	30	40		
				kN/m <sup>2</sup>					
				20	40	60	80	BLOWS/FT. (0.3m)	
SW	SAND, coarse, gravelly, fill	0.5	6.7						30/45
SP	SAND, fine, silty, brown; some silt near top of layer; some fine to medium sand in sample at 1.5 m	2.1	5.1						0/45
		4							13/45
		6							18/45
		8							8/45
GW, SW	GRAVEL, sandy, grey, slightly silty and SAND, gravelly, coarse, grey, slightly silty								
	Below 4 m is sand with many gravelly layers	10							
	Below 12.2 m, sand becomes fine to medium	12							
		13.7	-6.5						
	Bottom of hole, elev -6.5								
	Hole drilled to 3 m with difficulty, using casing								
	Installed piezometer, tip at depth 2.5 to 3.4 m								
	Moved 3 m and drilled to 5 m using mud and sampled at 2 to 5 m. Drilled to 13.7 m using mud								
	No permeability test as casing was loose in hole								







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## LOG OF DRILL HOLE

HOLE NO. DH 6

SHEET 1 OF 1

PROJECT ABBOTSFORD  
 LOCATION OF HOLE Chainage  
                           26+43.6  
 ELEVATION 5.17  
 CONTRACTOR Keller Soiltest  
 TYPE OF DRILL Hayhew 1000  
 DATE OF DRILLING 1 Feb 1977

### LEGEND

- SPLIT SPOON
- WASH SAMPLE
- SHELBY TUBE
- CORE SAMPLE

### SHEAR STRENGTH

- UNCONFINED COMPRESSION
- TORVANE
- PENETRATION RESISTANCE
- STANDARD N-VALUE
- ATTERBERG LIMITS

P.L. 
←
→
 L.L.  
 MOISTURE CONTENT

SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS				SAMPLE NO.	RECOVERY cm
				10	20	30	40		
				kN/m <sup>2</sup>					
				20    40    60    80					
				BLOWS/FT. (0.3 m)					
SW	SAND, well-graded, silty, gravelly, with cobbles; brown, FILL	1.5 2	-3.7						13/45
SW	SAND, well-graded, gravelly, silty	4							18/45
	Thin layer of silt at top of layer; some silty fine to medium sand in sample at 4.6 m	5.1 6	0.1						18/45
	Bottom of hole, elev 0.1								
	Installed standpipe piezometer, tip at depth 1.8 to 2.9 m								
	No permeability test carried out. Had much difficulty cleaning out casing, and return water flowed outside casing								







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NORTH VANCOUVER B.C.

HOLE NO. DH 8

SHEET 1 OF 1

## LOG OF DRILL HOLE

PROJECT ABBOTSFORD  
 LOCATION OF HOLE Chainage  
                           39+89.4  
 ELEVATION 4.68  
 CONTRACTOR Keller Soiltest  
 TYPE OF DRILL Mayhew 1000  
 DATE OF DRILLING 31 Jan 1977

### LEGEND

- SPLIT SPOON
- WASH SAMPLE
- SHELBY TUBE
- CORE SAMPLE

### SHEAR STRENGTH

- UNCONFINED COMPRESSION
- TORVANE
- PENETRATION RESISTANCE
- STANDARD N-VALUE
- ATTERBERG LIMITS

P.L. 
←
→
 L.L.  
 MOISTURE CONTENT

SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS								SAMPLE NO.	RECOVERY cm
				10	20	30	40	kN/m <sup>2</sup>		BLOWS/FT. (0.3 m)			
				20	40	60	80						
SW, SM	SAND, silty, gravelly, with cobbles, brown; angular particles; fill	1.5	3.2										5/45
SP	SAND, fine, silty, grey; with thin layers of silt	2.7	2.0										46/60
		4											0/45
SW	SAND, well graded, gravelly, coarse	5.1	0.4										10/45
	Bottom of hole, elev -0.4 Installed standpipe piezo- meter, tip at depth 2.9 to 3.8 m  No permeability test; casing used to depth 4.4 m, but was loose in hole  Lost 1.5 m length of casing and casing shoe  Sample at 0 to 0.9 m taken from material dug out of hole by hand												







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HOLE NO. DH 11

SHEET 1 OF 1

## LOG OF DRILL HOLE

PROJECT ABBOTSFORD  
 LOCATION OF HOLE Chainage  
62+41.7  
 ELEVATION 5.10  
 CONTRACTOR Keller Soiltest  
 TYPE OF DRILL Mayhew 1000  
 DATE OF DRILLING 20 Jan 1977

### LEGEND

- SPLIT SPOON
- WASH SAMPLE
- SHELBY TUBE
- CORE SAMPLE

- ### SHEAR STRENGTH
- UNCONFINED COMPRESSION
  - TORVANE
  - PENETRATION RESISTANCE
  - STANDARD N-VALUE
  - ATTERBERG LIMITS

P.L. 
|
|
 L.L.  
 MOISTURE CONTENT

SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS				SAMPLE NO.	RECOVERY cm
				10	20	30	40		
				kN/m <sup>2</sup>					
				BLOWS/FT. (0.3 m)					
				20	40	60	80		
SG	SAND, gravelly, with cobbles, silty, brown; fill	0.6	4.5						
SP		1.5	3.6						30/45
CL	SAND, fine to medium, fill								
	CLAY, brown to grey, many rust spots	3.0	2.1						10/60
SP	SAND, fine to medium; silty at top of layer, some coarse sand, trace roots, trace gravel	5.0	0.1						45/45
	Bottom of hole, elev. 0.1								
	Installed standpipe piezometer, tip at depth 4.0 to 4.8 m.								
	Conducted permeability test, casing to depth 2.7 m, hole open to 4.8 m; calculated $k = 1.1 \times 10^{-4}$ cm/sec.								





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## LOG OF DRILL HOLE

HOLE NO. DH 13

SHEET 1 OF 1

PROJECT ABBOTSFORD  
 LOCATION OF HOLE Chainage  
74+09.0  
 ELEVATION 5.56  
 CONTRACTOR Keller Soiltest  
 TYPE OF DRILL Mayhew 1000  
 DATE OF DRILLING 26 Jan 1977

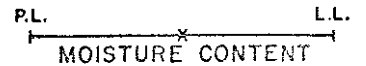
### LEGEND

- ☐ SPLIT SPOON
- ☒ WASH SAMPLE
- ☒ SHELBY TUBE
- ☐ CORE SAMPLE

### SHEAR STRENGTH

- ⊕ UNCONFINED COMPRESSION
- + TORVANE
- PENETRATION RESISTANCE
- ⊙ STANDARD N-VALUE

### ATTERBERG LIMITS



SYMBOL	DESCRIPTION	DEPTH METRES	ELEV. METRES	TEST RESULTS				SAMPLE NO.	RECOVERY cm
				10	20	30	40		
				kN/m <sup>2</sup>					
				20	40	60	80	BLOWS/FT. (0.3m)	
SG	SAND, brown, gravelly, silty, fill	0.6	5.0						
ML	SILT, brown to grey at depth, trace roots; many rust coloured spots near top of layer. Many thin layers of fine sand at depth.	2							36/45
		4							53/60
									45/45
									60/60
SP	SAND, fine to medium, trace of roots. Gravelly below 6.7 m.	5.8	-0.2						
		7.0	-1.4						30/45
	Bottom of hole, elev. -1.4								
	Installed standpipe piezometer, tip at depth 5.7 to 7.0 m.								
	Falling head permeability test conducted with casing to depth 3.0 m, hole open to 7.0 m. Calculated $k = 4.2 \times 10^{-4}$ cm/sec								